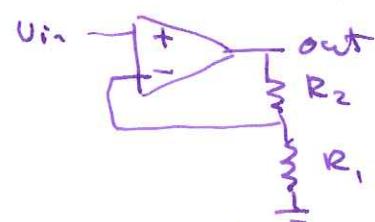


Feedback - some notation & algebra to show that "things get better if you 'throw away' gain"



$B$



$$A(v_{in} - Bv_{out}) = v_{out}$$

$$B = \frac{R_1}{R_1 + R_2}$$

Remark: not related to transistor  $\beta$

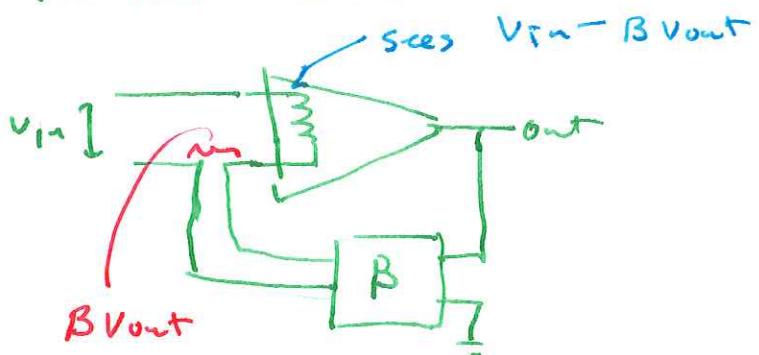
$$v_{in} = (B + \frac{1}{A}) v_{out}$$

$$\frac{1}{(B + \frac{1}{A})} = \frac{v_{out}}{v_{in}} \leftarrow \begin{array}{l} \text{circuit} \\ \text{gain} \end{array} \quad \left. \begin{array}{l} \text{in contrast to opamps} \\ \text{gain} \end{array} \right\}$$

$$\frac{1}{(1 + \frac{1}{AB})} \leftarrow \frac{R_1 + R_2}{R_1} = 1 + \frac{R_2}{R_1}$$

sometimes called the "loop gain"  $A_B$

quadratic form



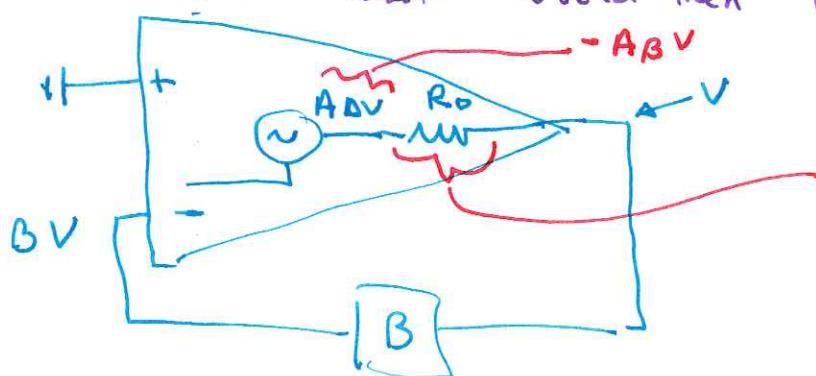
Note: the above is negative feedback; positive

feedback → expo growth and is generally a bad idea.

The invention of negative feedback amps is attributed to Harold Black - EE workers at Bell Labs - 1927

Output Impedance - a trick to mathematically calculate a circuit output impedance. Consider  $V_{in}=0$  ("ground the input") thus (in theory) would produce  $V_{out}=0$  but we (mathematically) apply an external voltage  $V$  to the output & calculate the resulting current,  $I$ . The circuit's output impedance is the  $\frac{V}{I}$ .

(In an experimental situation which more like remove current from amp - by adding a load - and measure the resulting voltage drop = the circuit's  $Z_{out}$  would then be  $\frac{\Delta V}{I}$ )

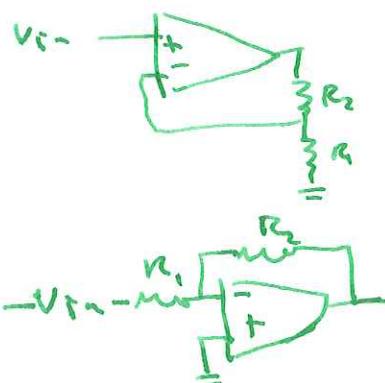


$$\text{voltage drop} = V - -ABV \\ = (1+AB)V$$

$$\text{current} = \frac{\text{voltage drop}}{R_o}$$

$$Z_o = \frac{V}{I} = \frac{R_o}{(1+AB)} \leftarrow \begin{array}{l} \text{note reduced} \\ \text{from what was} \\ \text{probably a small} \\ R_o to begin with. \end{array} \quad I = \frac{(1+AB)V}{R_o}$$

Slight practical consideration - in real circuit feedback network  $B$  it self would draw some current

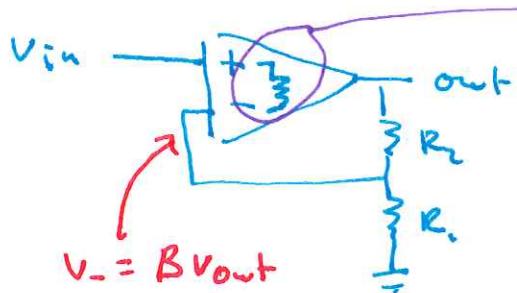


in both cases an addition current flow of  $\frac{V}{R_1+R_2}$  happens - i.e. must add this current to above

$$\text{result: } Z_{out} = \frac{R_o}{(1+AB)} \parallel R_1 + R_2$$

this should be much smaller than  $R_1 + R_2$  so  
 $Z_o \approx R_o / (1+AB)$

Input Impedance (Note: for inverting amp circuit this will be  $R_i$  which is not true — say  $k\Omega$ )



$$V_- = BV_{out}$$

$$B = \frac{R_f}{R_i + R_2}$$

$$I = \frac{V_{in} - BV_{out}}{R_{in}} = \frac{V_{in}}{R_{in}} (1 - BG)$$

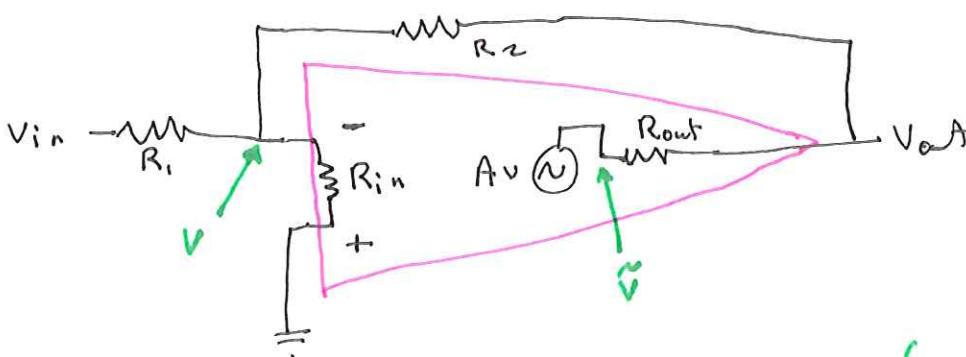
$$G = \frac{V_{out}}{V_{in}} = \frac{A}{1 + BA}$$

$$\frac{V_{in}}{I} = \frac{R_{in}}{(1 - BG)} = \frac{R_{in}}{\left(1 - \frac{AB}{1 + BA}\right)}$$

$$= \underline{R_{in}(1 + BA)}$$

an internally large value increased even more.

# Inverting Amp: Input/Output Impedance



open loop gain  $A$   
 closed loop gain  $G = \frac{V_o}{V_i}$   
 loop gain  $A \cdot B$   
 $B = \frac{R_1}{R_1 + R_2}$

$$V = \frac{\frac{V_i}{R_1} + \frac{V_o}{R_2}}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_{in}}} = -\frac{1}{A} V_o \Rightarrow \frac{\frac{1}{R_1} + \frac{G}{R_2}}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_{in}}} = -\frac{G}{A}$$

math  $\Rightarrow G = -\left( \frac{A R_2 R_{in}}{R_1 R_2 + R_{in} R_1 (A+1) + R_{in} R_2} \right)$

$$\xrightarrow{R_{in} \rightarrow \infty} \frac{-A R_2}{R_1 (A+1) + R_2} = \frac{-A (1-B)}{AB + 1} \xrightarrow{A \rightarrow \infty} \frac{-(1-B)}{B} = -\frac{R_2}{R_1}$$

$$I_{in} = \frac{(V_{in} - V)}{R_1} = \frac{(V_{in} + \frac{1}{A} V_{out})}{R_1} = \frac{V_{in} (1 + \frac{G}{A})}{R_1}$$

$$\frac{R_1}{(1 + G/A)} = \frac{V_{in}}{I_{in}} = R_1 + R_{in} \parallel \frac{R_2}{(1+B)} \quad (\text{math})$$

Ignore  $R_{in}$ , Ground  $V_{in}$ , Apply voltage  $V_o$  to output, measure current  $I_o$

$$V = \frac{V_o}{R_2} ; \quad -A V = \tilde{V}$$

$$I_{out} = \frac{(\tilde{V} - V_o)}{R_{out}} = \frac{-V_o}{R_{out}} \left\{ \frac{\frac{A}{R_2}}{\frac{1}{R_1} + \frac{1}{R_2}} + 1 \right\}$$

$$\left\{ \frac{R_{out}}{\frac{A/R_2}{1/R_1 + 1/R_2} + 1} \right\} = \frac{-V_o}{I_{out}} = \frac{R_{out}}{AB + 1}$$

$$\underbrace{\frac{A R_1}{R_2 + R_1} + 1}_{=} = AB + 1$$

```
Solve[(1/R1+G/R2)/(1/R1+1/R2+1/Ri)==-G/A,G]
```

$$\text{Out}[1]= \left\{ \left\{ G \rightarrow -\left( \frac{A R_2 R_i}{R_1 R_2 + R_1 R_i + A R_1 R_i + R_2 R_i} \right) \right\} \right\}$$

```
R1/(1+G/A) /. First[%]
```

```
Simplify[%]
```

$$\text{Out}[3]= \frac{R_2 R_i + R_1 (R_2 + R_i + A R_i)}{R_2 + R_i + A R_i}$$

```
R1+Ri R2/(1+A)/(Ri+R2/(1+A))
```

```
Simplify[%]
```

$$\text{Out}[5]= \frac{R_2 R_i + R_1 (R_2 + R_i + A R_i)}{R_2 + R_i + A R_i}$$

## Vocabulary

AC or DC amp

bandwidth ( $f_{-3dB}$ ) ; "mid band" gain

inverting/ non inverting

clipping

differential amp ( $\text{out} = A_d(V_+ - V_-)$ )

- common mode gain (where  $V_+ = V_- = V_{\text{ref}}$ )  $A_c$

- differential gain (where  $V_+ - V_- = V_{\text{ref}}$ )  $A_d$

- common mode rejection ratio =  $\frac{A_d}{A_c}$  (often in dB)

noise - note odd unit  $\mu\text{V}/\sqrt{\text{Hz}}$  or  $\text{PA}/\sqrt{\text{Hz}}$

## For op-Amps

Gain-Bandwidth product [note Compensated op-Amps]

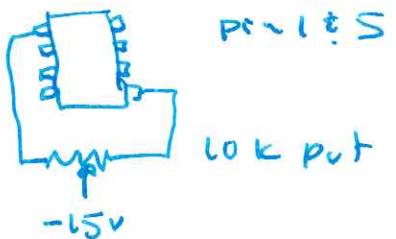
Stev rate

"rail-to-rail" or limited output voltage swing

input offset voltage - "as if"

input bias current

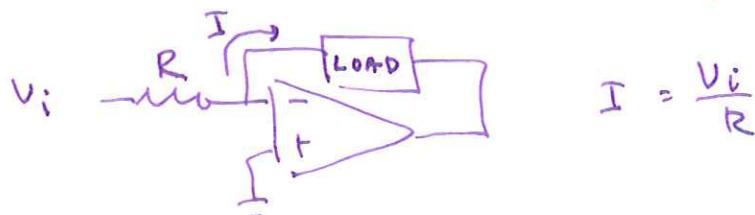
open loop gain



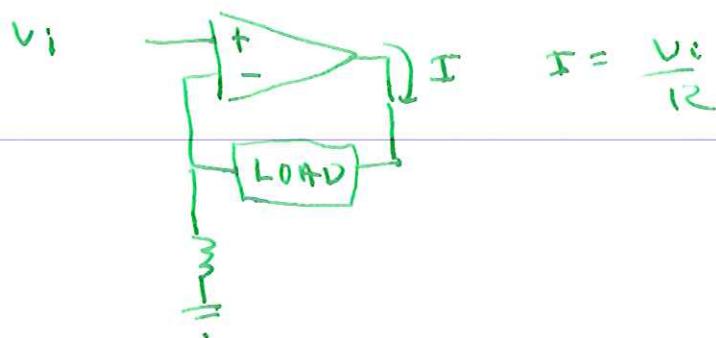
Current sources — supplies a fixed current — if  $R \rightarrow \text{big}$   
 a big voltage results; if  $R$  small  $\rightarrow$  small voltage.

Every current source has its limits — if  $R$  is too big  
 will not be able to produce required voltage.

[contrast: voltage sources supply fixed voltage — if  $R$  is  
 big a small current results; if  $R$  small  $\rightarrow$  large current.  
 Every voltage source has its limits — if  $R$  is too small  
 will not be able to produce required current]

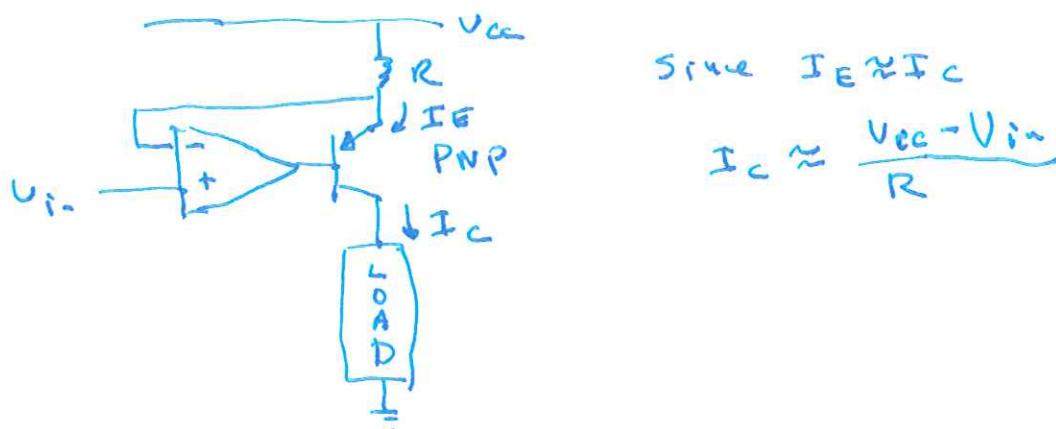


$$I = \frac{V_i}{R}$$



$$I = \frac{V_i}{R}$$

Above require a "floating" load — often want load  
 connected to ground. Also above limited by current  
 output of op-amp  $\rightarrow$  a few mA



Since  $I_E \approx I_C$

$$I_C \approx \frac{V_{cc} - V_{in}}{R}$$